



**Measurement of Beacon Anisoplanatism Through a  
Two-Dimensional, Weakly-Compressible Shear Layer**

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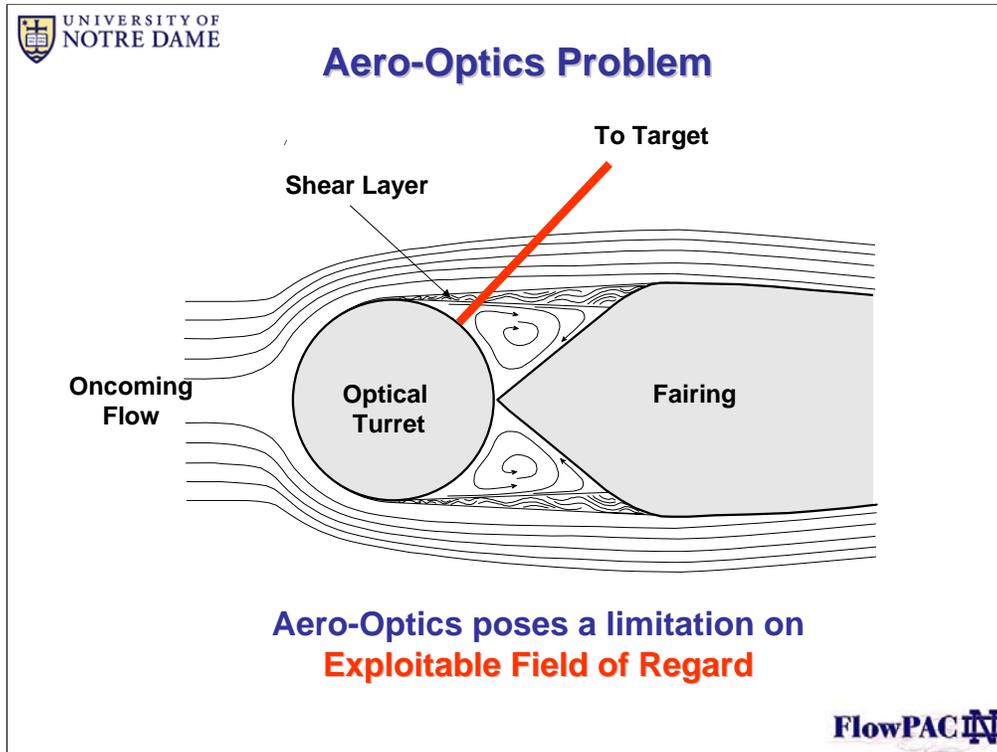
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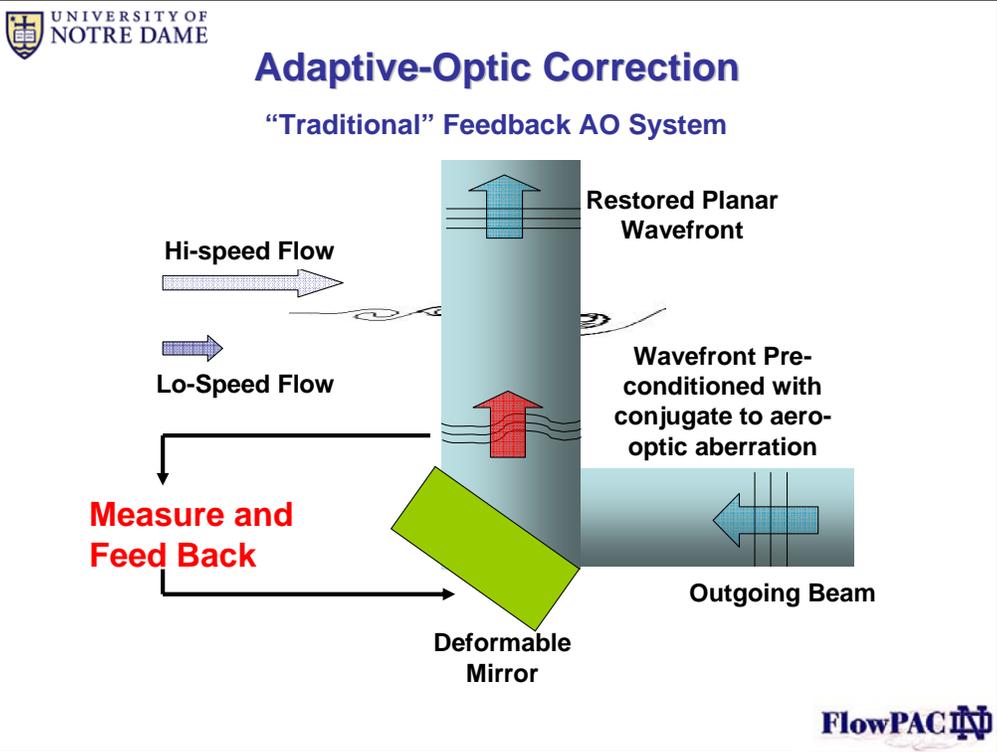
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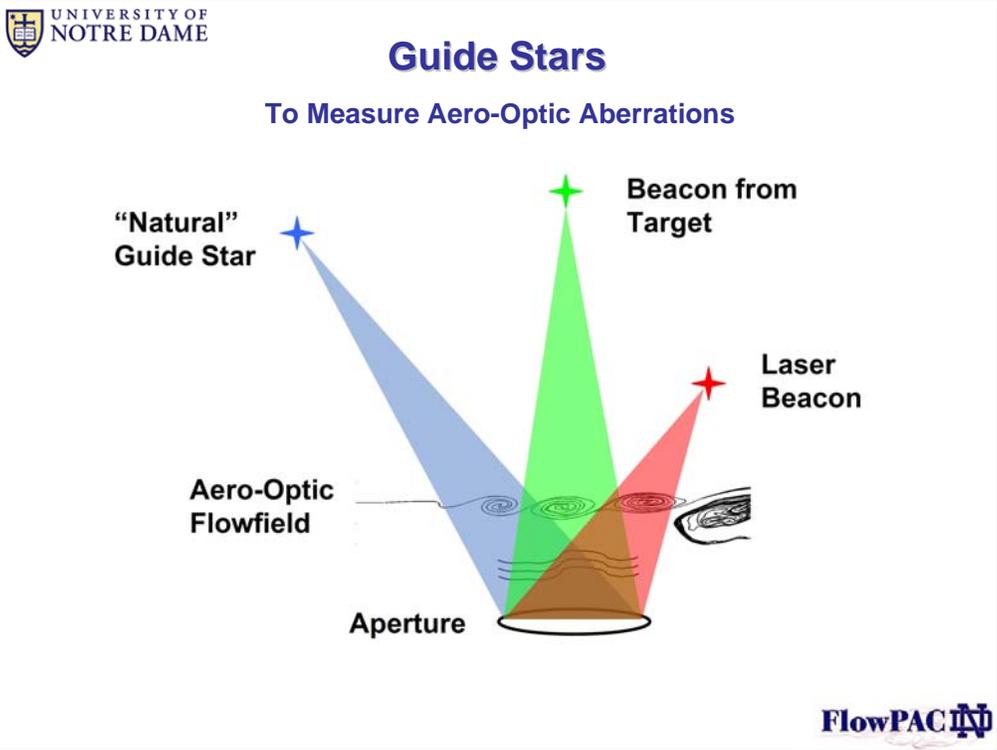




- General definition of the aero-optics problem
- For aft-pointing direction, beam typically passes through a separated shear layer – aero-optic aberrations
- Aero-optics therefore poses a limitation on exploitable field of regard

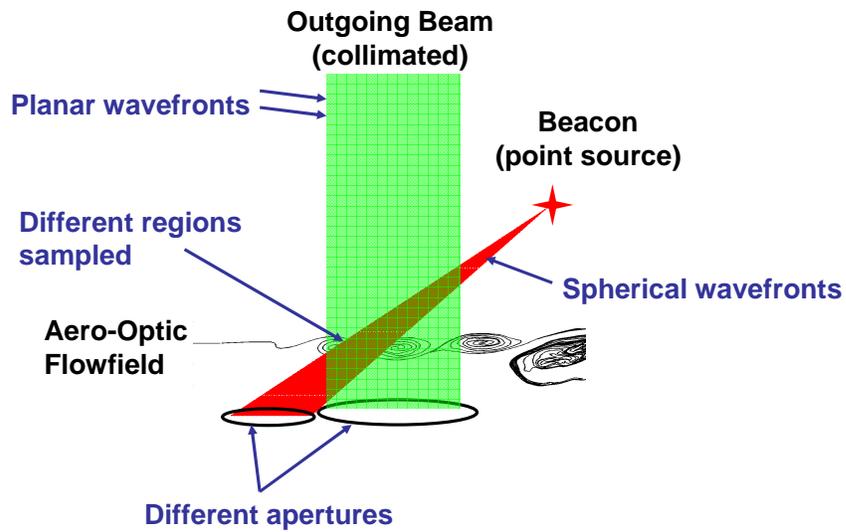


- Aero-optic aberrations can be corrected using adaptive-optic system
- (read slide)
- Key is that aero-optic aberrations must be measured in order to close the feedback loop



- One way to measure aero-optic aberration is using guide stars
- Examples include ... (read slide)
- Most reliable is probably the artificially-created near-field beacon; our research focuses on this option

## Anisoplanatic Effects



- When a beacon is used, problems arise in the form of anisoplanatism between the beacon and the outgoing beam that is being corrected
- Anisoplanatic effects include, for example, different regions sampled, different wavefront shapes, different apertures

## Objectives

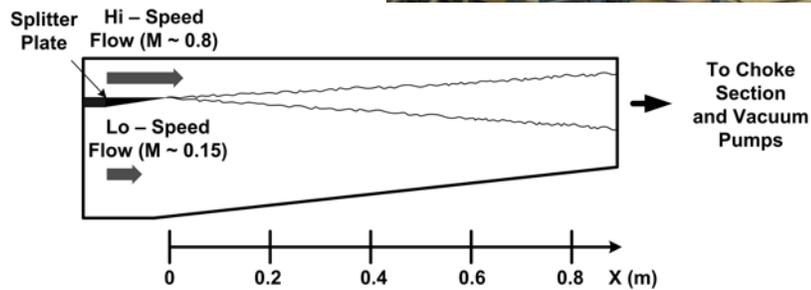
1. Design an experiment that incorporates significant anisoplanatism
2. Test whether anisoplanatic effects can be mitigated using a “Minimum Mean Square Estimation” (MMSE) Approach

Objectives of this research are therefore ... (read slide)

## Wind Tunnel



### Test Section:

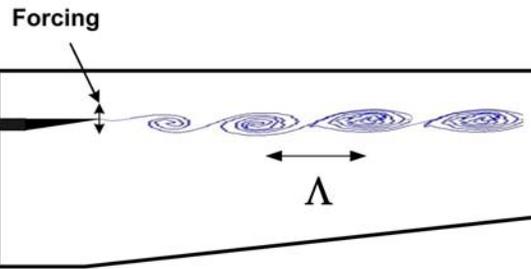


FlowPAC 

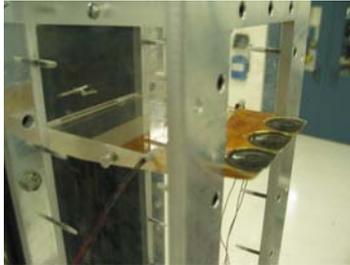
Experimental investigation using ND's Compressible Shear-Layer Wind Tunnel

- Experimental flowfield models aero-optic environment of a separated shear layer
- Indraft configuration with separate inlets for high-speed and lo-speed flows
- Air drawn through TS, choke section and diffuser to pumps located behind wall
- 0.9 m long test section, contracts slightly to reproduce conditions of unconstrained flow

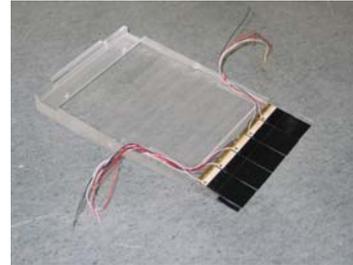
## Shear-Layer Forcing



Voice-Coil



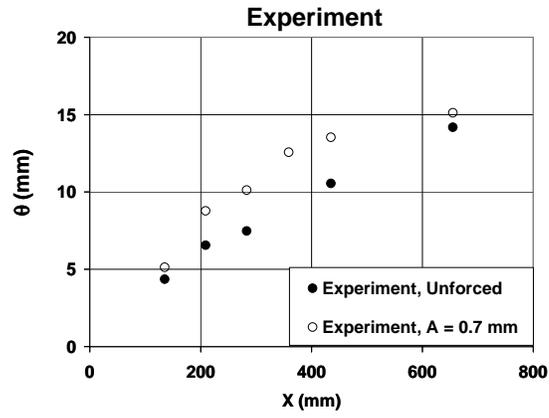
Piezoelectric



We also have capability to force the shear layer

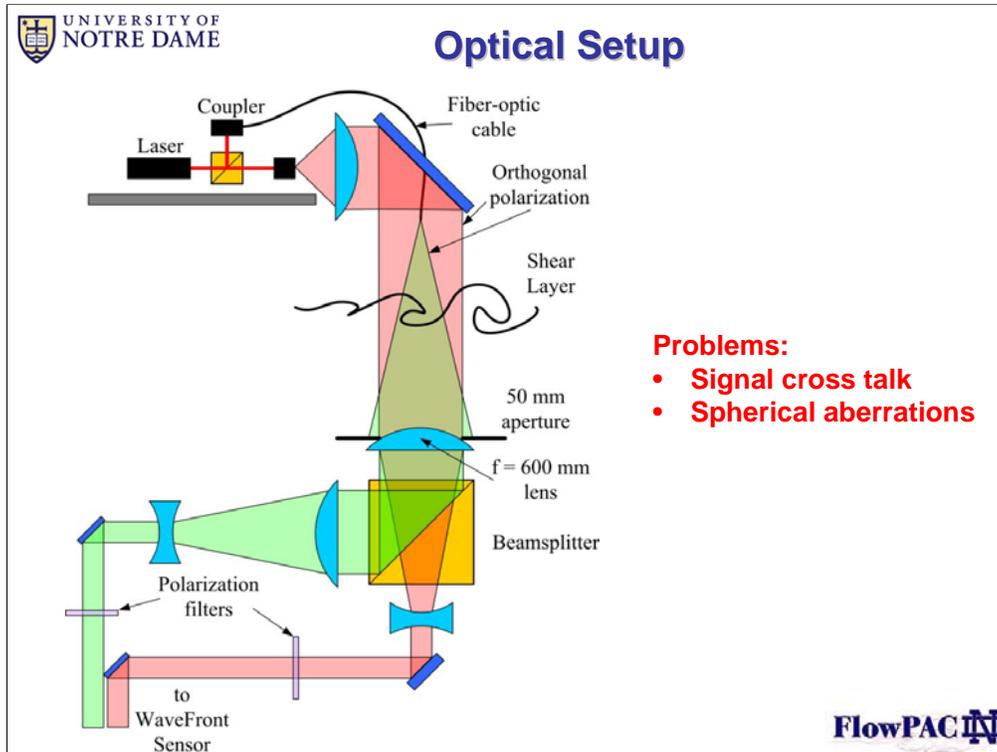
- Regularizes shear layer
- Larger-amplitude aberrations (signal to noise)
- Two types of forcing actuators

## Forced Shear Layer Growth



This shows the effect of forcing.

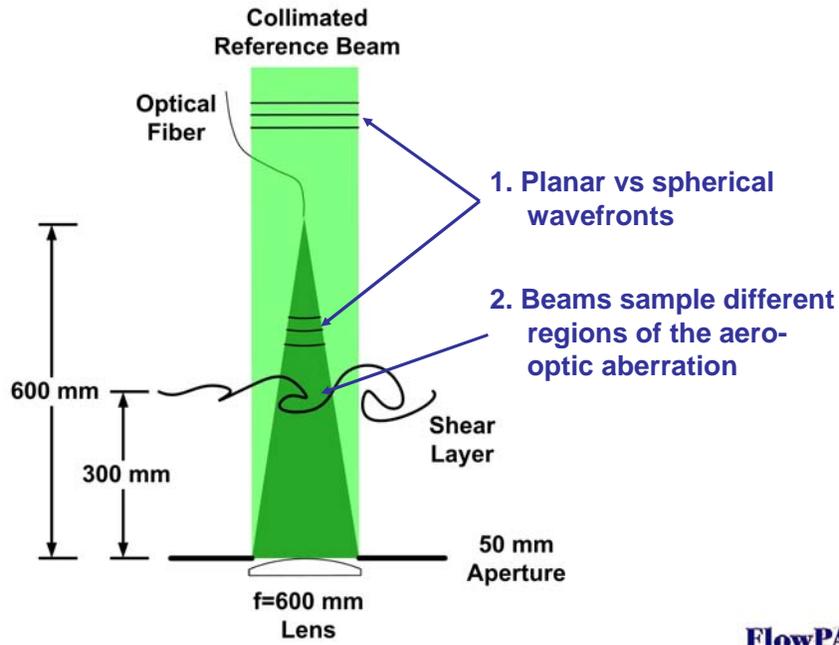
For our application, primarily interested in increasing the amplitude of shear-layer aberrations, as indicated by increased momentum thickness



## Optical setup

- Pulsed YAG laser f-doubled to 532 nm
- Split into collimated reference, diverging beacon beams
- For beacon, used output of an optical fiber (3.6  $\mu\text{m}$  dia effectively a point source)
- Passed co-axially thru shear layer
- Collected with f600 mm lens apertured to 50 mm
- Reason for 50 mm aperture is size limit on beamsplitter (didn't have time for larger custom beamsplitters)
- Beams reduced and oriented parallel into WFS
- Crosstalk eliminated by orthogonal polarization of beams, but in practice this was negligible due to different wavefront shape of beams
- Talk about spherical aberrations later

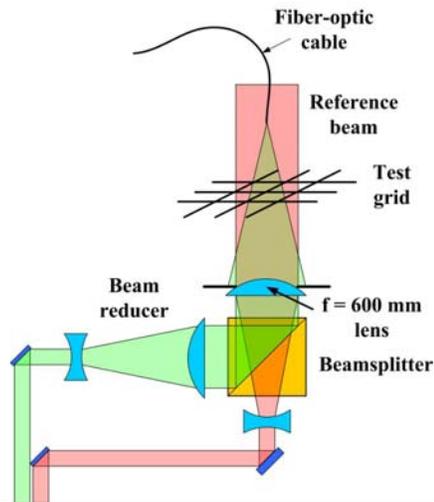
# Anisoplanatism



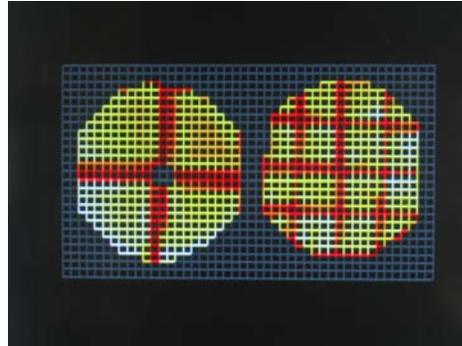
Anisoplanatism effects (read slide)

## Image Quality/ Spherical Aberrations

- Extra care with lens selection and orientation
- “Staged” beam expanders
- Minimized beam path lengths



WFS Image:



FlowPAC 

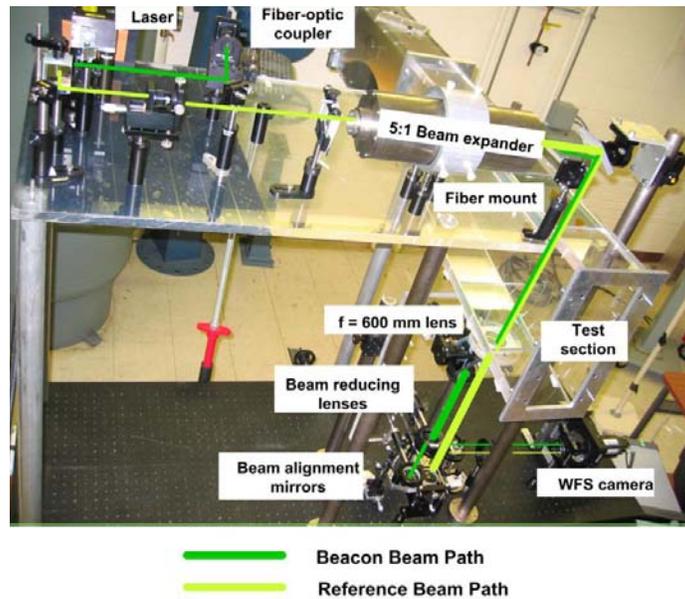
The anisoplanatism analysis compares spatial details of reference and beacon beams and this means that minimizing spherical aberrations to improve image quality is a big issue.

Spherical aberrations reduced by ... (read slide)

Example image of test grid (course image since it was acquired thru lenslet array of WFS)

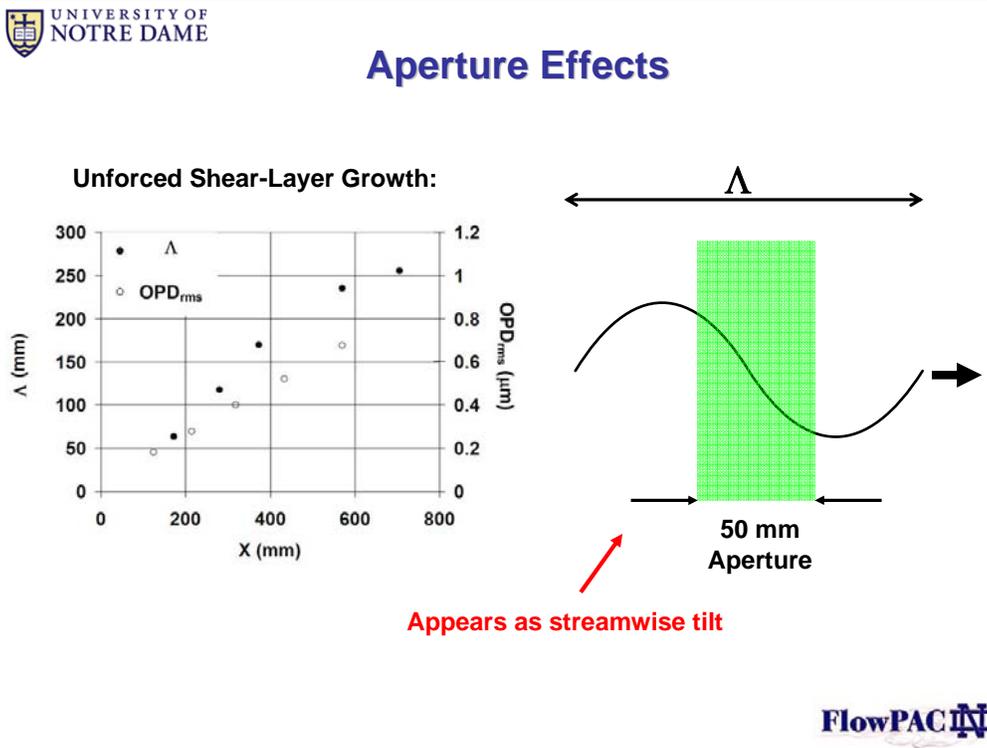
- No noticeable spatial distortions
- Beacon maps to inner 50% of reference

## Photograph of Experiment



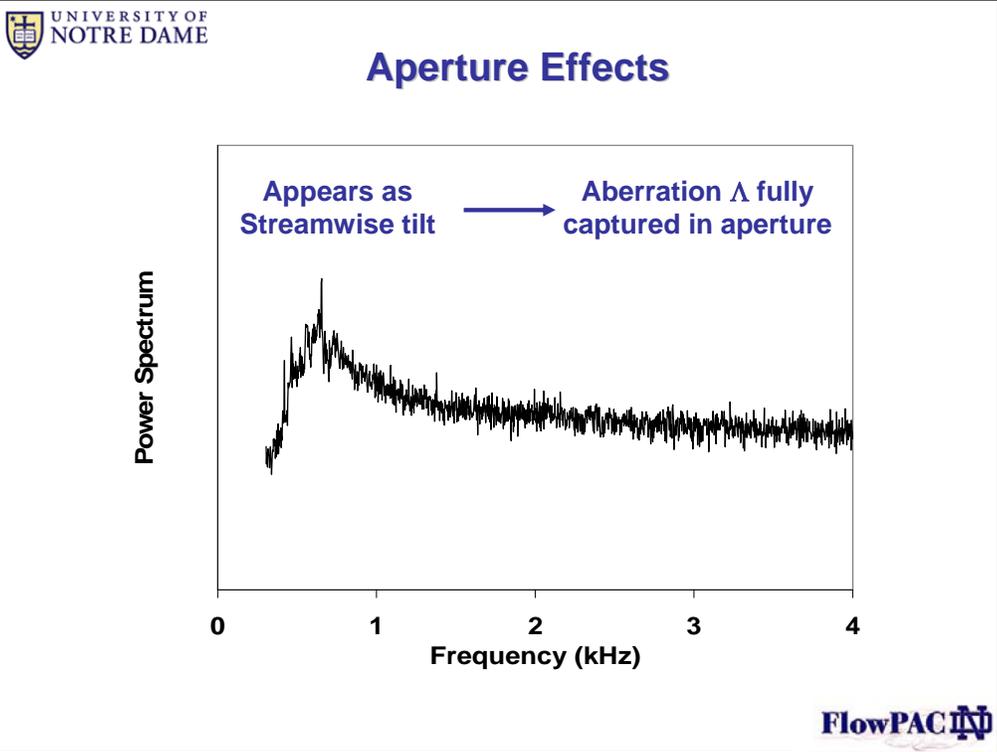
Picture of final experimental layout

- Laser, beam expanders for reference beam and fiber-optic coupler located on raised platform above test section
- F600mm lens located beneath test section
- Beam reducers and alignment mirrors below test section
- WFS camera



Comment on aperture effects

- Dominant shear-layer structure size and aberration strength both grow with downstream distance
- Favorable to run experiments farther downstream where aberrations are strong (better s/n)
- However, longer downstream aberration scales mostly as streamwise tilt in 50 mm aperture



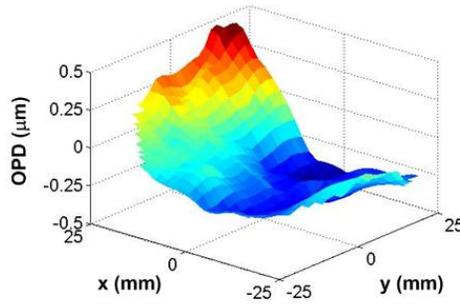
Power spectrum shows that strongest aberrations appear as streamwise tilt. Only higher-frequency aberrations are fully captured in the aperture.

Therefore ran at several downstream locations, with and without forcing to generate different conditions.

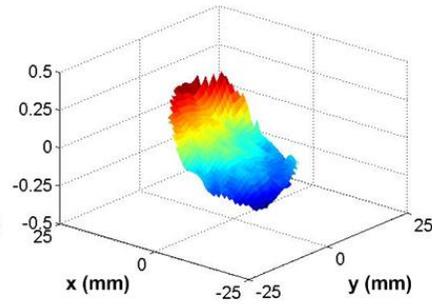
## Example Wavefronts

$x = 300$  mm, Shear layer forced at 750 Hz

Reference Beam:



Beacon Beam:

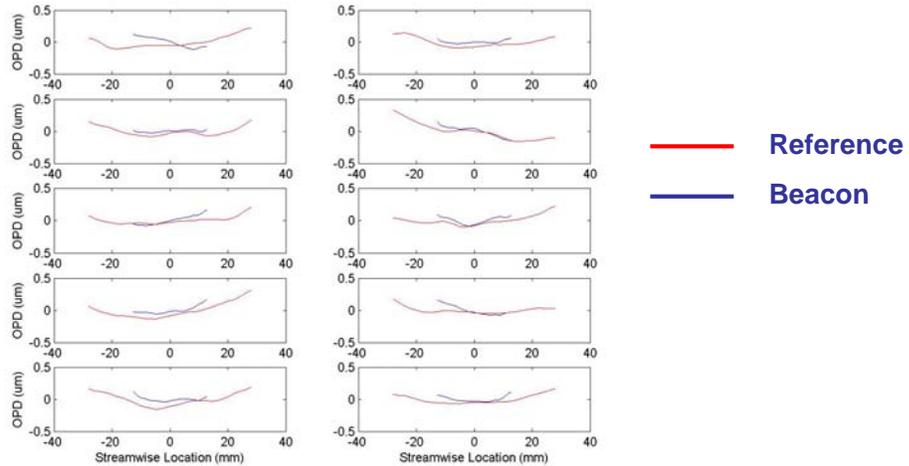


### Example wavefronts

- Mostly streamwise tilt
- Beacon matches the inner ~50% of reference beam
- Aberrations appear fairly 2-D

## Example Wavefronts

Wavefronts Averaged in Cross-Stream Direction



Slide shows several other example wavefronts, averaged in cross-stream dimension since wavefronts have 2-D appearance

## Mitigation of Anisoplanatism

### Linear Estimation Theory

Define:

$$\hat{C}_h = \mathbf{A} C_m$$

Minimal Mean-Square  
Estimation (MMSE)

Determine  $\mathbf{A}$  that minimizes difference between  
measured and estimated reference wavefront

$$\text{diag} [ (C_h - \hat{C}_h)(C_h - \hat{C}_h)^T ] = \text{diag}[ C_h C_h^T - \mathbf{B} \mathbf{C}^{-1} \mathbf{B}^T ]$$

where:

$$\mathbf{A} = \mathbf{B} \mathbf{C}^{-1} \quad \mathbf{B} = \langle C_h C_m^T \rangle \quad \mathbf{C} = \langle C_m C_m^T \rangle$$

Linear estimation theory used to mitigate anisoplanatism between beacon and reference beams

- Define an estimate for the reference wavefront that will be computed from the measured data using an estimation matrix  $\mathbf{A}$
- Determine  $\mathbf{A}$  that minimizes ... (read slide)
- This is satisfied when ...
- Where these matrices are defined as ...

## Mitigation of Anisoplanatism

### Procedure

“Anisoplanatism”:

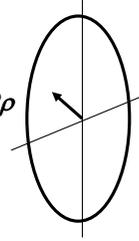
$$\varepsilon_{hb}^2 = \int d\rho W(\rho) \langle [\phi_h(R\rho) - \phi_b(R\rho)]^2 \rangle$$

Compute estimated reference wavefront using MMSE

Compute anisoplanatic residual:

$$\widehat{\varepsilon}_{hb}^2 = \int d\rho W(\rho) \langle [\phi_h(R\rho) - \widehat{\phi}_h(R\rho)]^2 \rangle$$

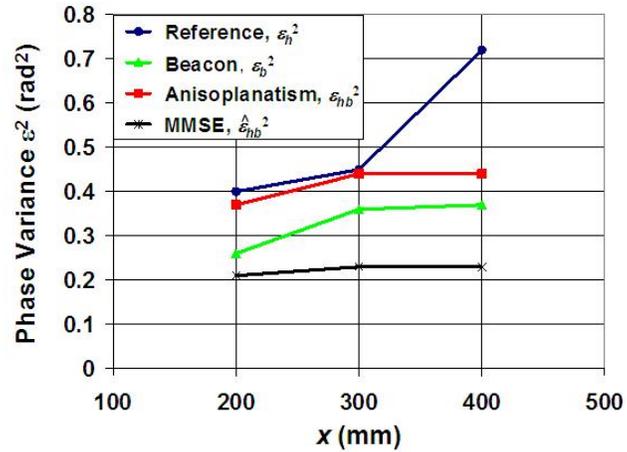
Aperture  
coordinates  $R\rho$



So our procedure to mitigate the anisoplanatism of the beacon measurements was as follows:

- Compute anisoplanatism
- Apply MMSE
- Compute residual anisoplanatism between reference beam and estimated reference

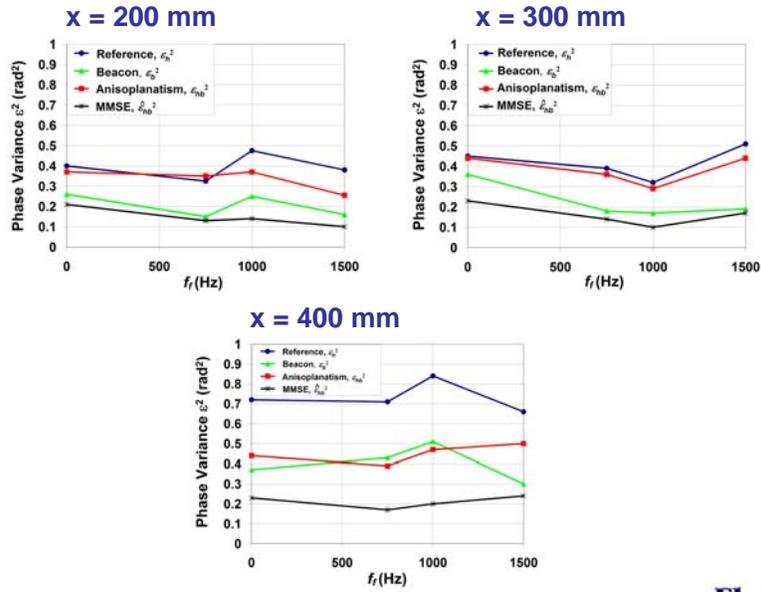
## Unforced Shear Layer



Results for unforced shear layer

- Anisoplanatism is nearly as large as variance on the original reference beam – hence attempting to correct reference beam using unmodified beacon measurements would introduce additional errors despite the similarity of the wavefronts shown earlier
- MMSE reduces anisoplanatism by ~50%

## Forced Shear Layer

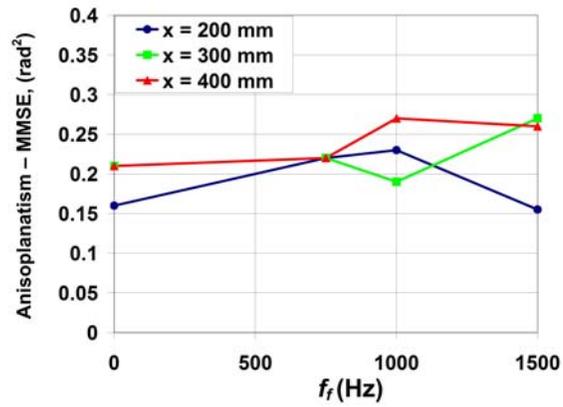


Forced shear layer

- Similar results with shear-layer forced
- Note slight improvement in MMSE with shear layer forced

## Summary

### Reduction in Anisoplanatism



Shows slight improvement in MMSE with shear-layer forced/regularized

- May be due to larger signal to noise
- Or due to regularization of shear layer

## Conclusions

1. Experiment design was successful in creating measurable anisoplanatism in a realistic aero-optic flow (compressible shear layer)
2. MMSE estimator reduced residual anisoplanatism to ~50% of initial value
3. Shear-layer forcing had a slightly beneficial effect on the ability of the MMSE estimator to correct the beacon wavefronts.

Conclusions ... (read slide)

## Future Work

1. More experimental data to more fully test the technique
2. Investigate guide stars from laser-induced air breakdown
  - Spark wavefront quality
  - Flow effects on breakdown spark
3. Investigate “realistic” flight applications

### Future Work

- We have recently been funded to carry on the investigation using actual laser-induced air breakdown rather than fiber-optic simulation
- “realistic” flight applications – “calibrate” a system and check performance in off-design conditions